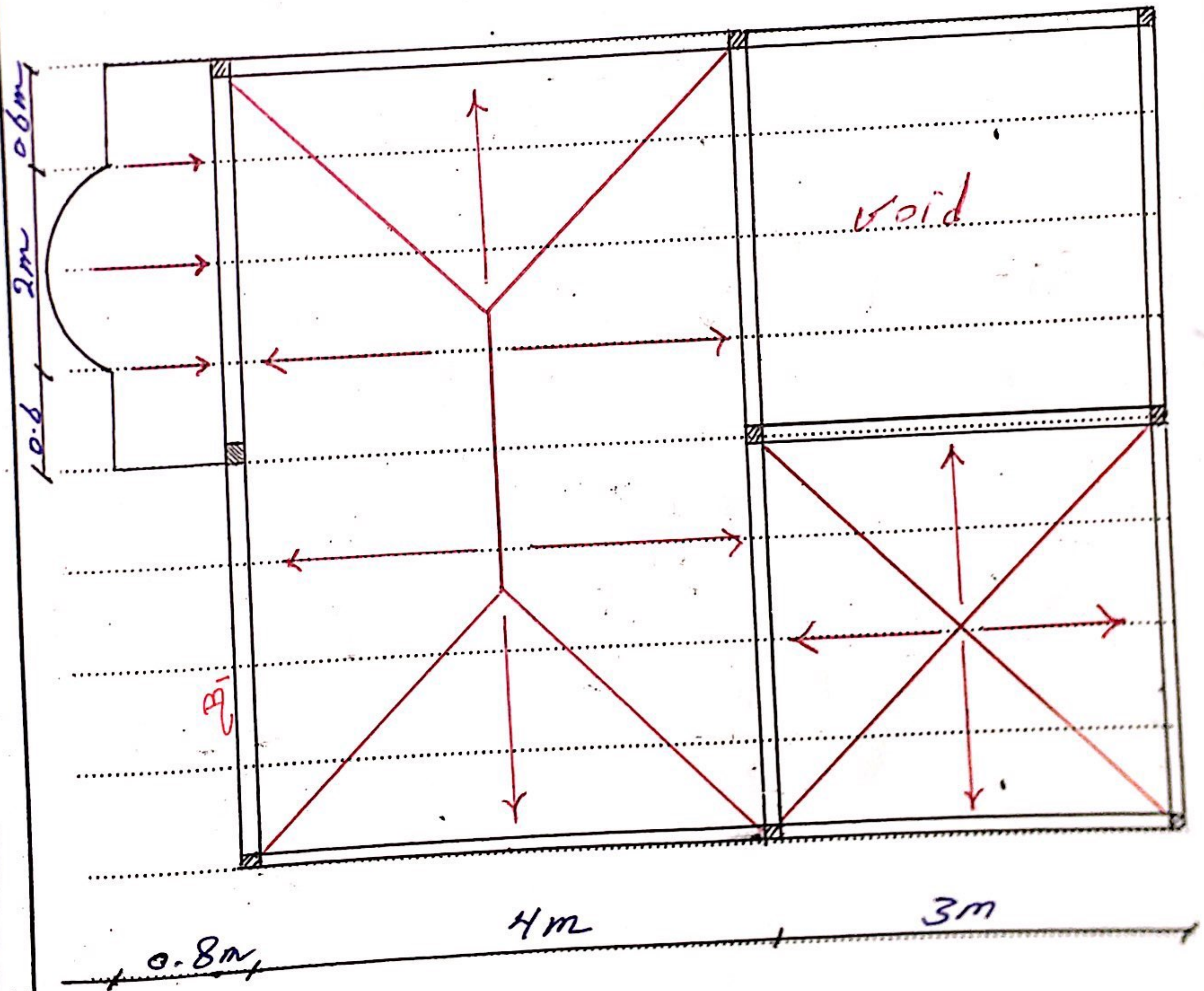


Eng.

# 'Model Answer'

D load dist For the plan:-



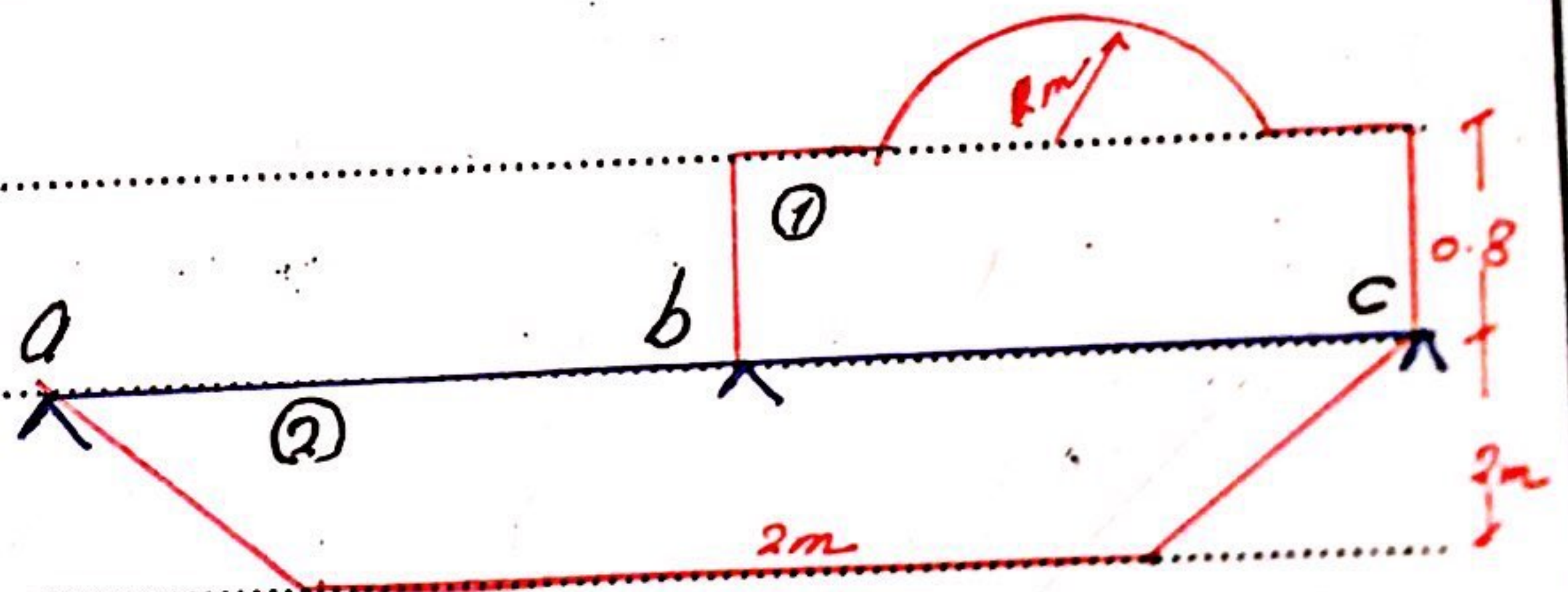
Eng.

→ o.w. of beams:  $a.w = b \pm \delta_{r.c}$   
 $= 0.25 \times 0.6 \times 25 = 3.75 \text{ kW/m}$

→ weight of wall  $= w_w = b_w h_w \delta_w$   
 $= (3 - 0.6) \times 2.5 = 6 \text{ kW/m}$

→ weight of slab  $= D.l_s = t_s \delta_c + f.c + o.p$   
 $= 0.14 \times 25 + 1.5 + 3 = 8 \text{ kW/m}^2$

For B<sub>1</sub>

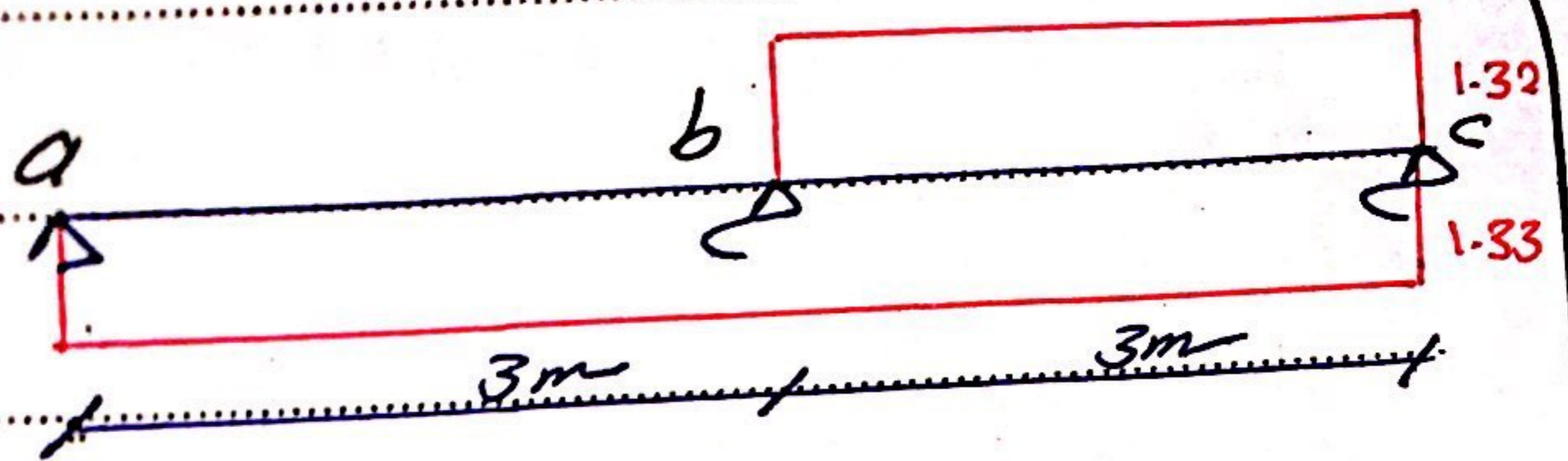


For shape ①  $h_{eq} = \frac{\Sigma \text{Area}}{\text{span}}$

$$= \frac{0.8 \times 3 + \frac{1}{2} \pi (1)^2}{3} = 1.32 \text{ m}$$

For shape ②

$$= \frac{\frac{2+3}{2} \times 2}{3} = 1.33 \text{ m}$$

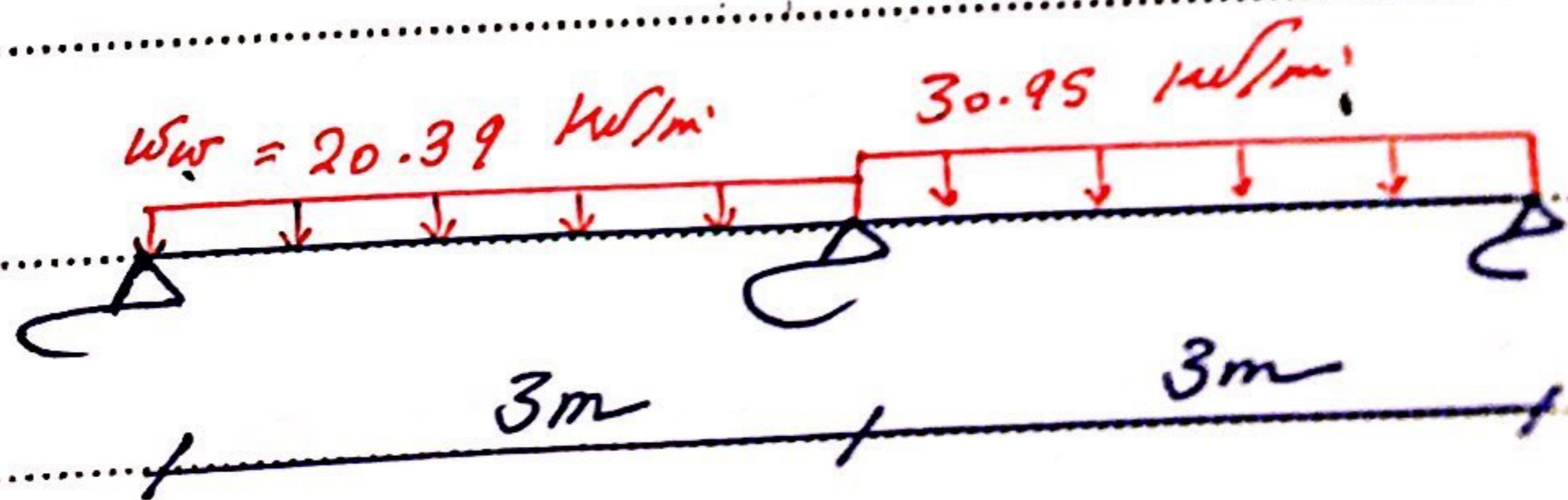


For part ab

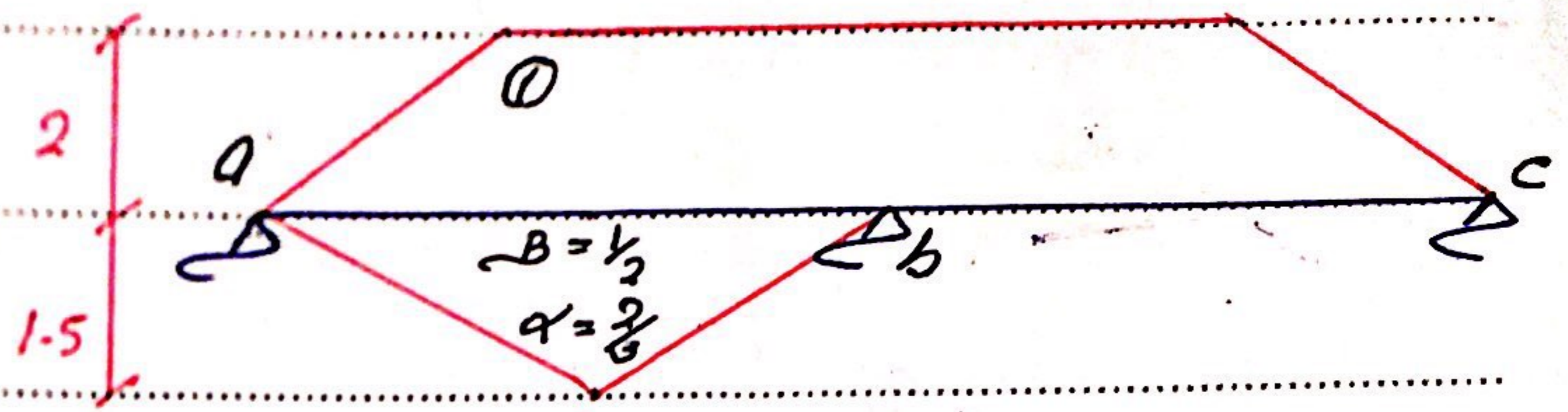
$$D.L = 3.75 + 6 + 8 \times 1.33 = 20.39 \text{ kN/m}$$

For part bc

$$U.L = 3.75 + 6 + 8(1.32 + 1.33) = 30.95 \text{ kN/m}$$



For  $B_2$



Key for shape 0  $h_{eq} = \frac{\frac{2+b}{2} \times 2}{b} = 1.33$

For part ab

Load for shear :-

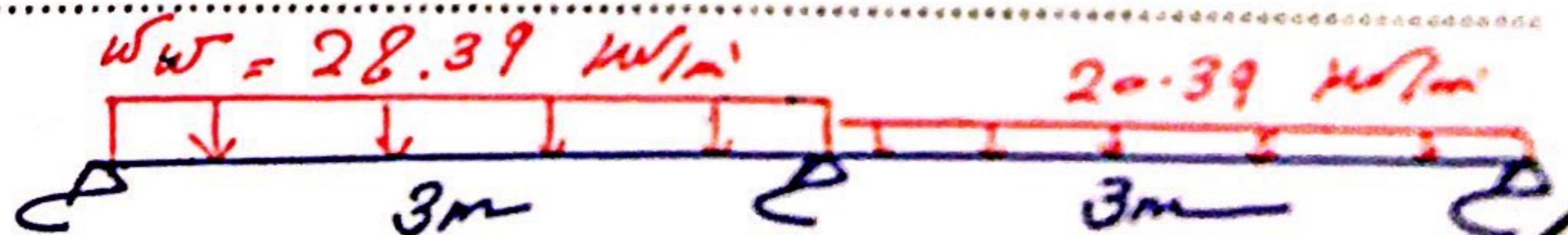
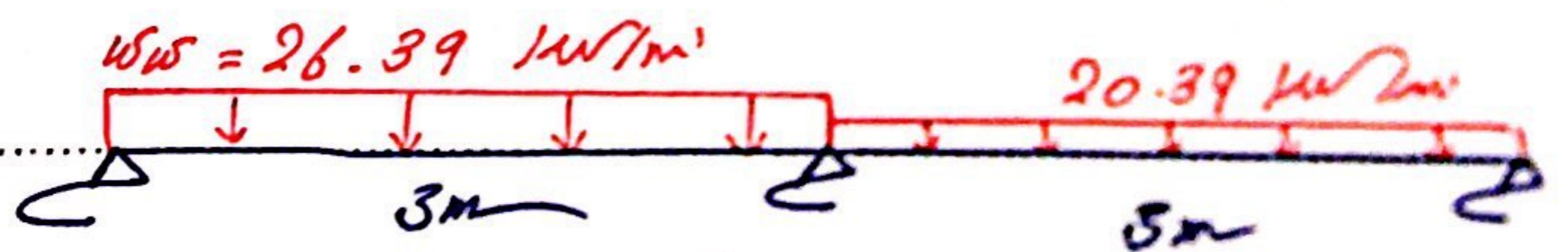
$$W_w = 3.75 + b + 8 \times 1.33 + 8 \times 1.5 \times \frac{1}{2} = 26.39 \text{ kN/m}$$

Load for normal :-

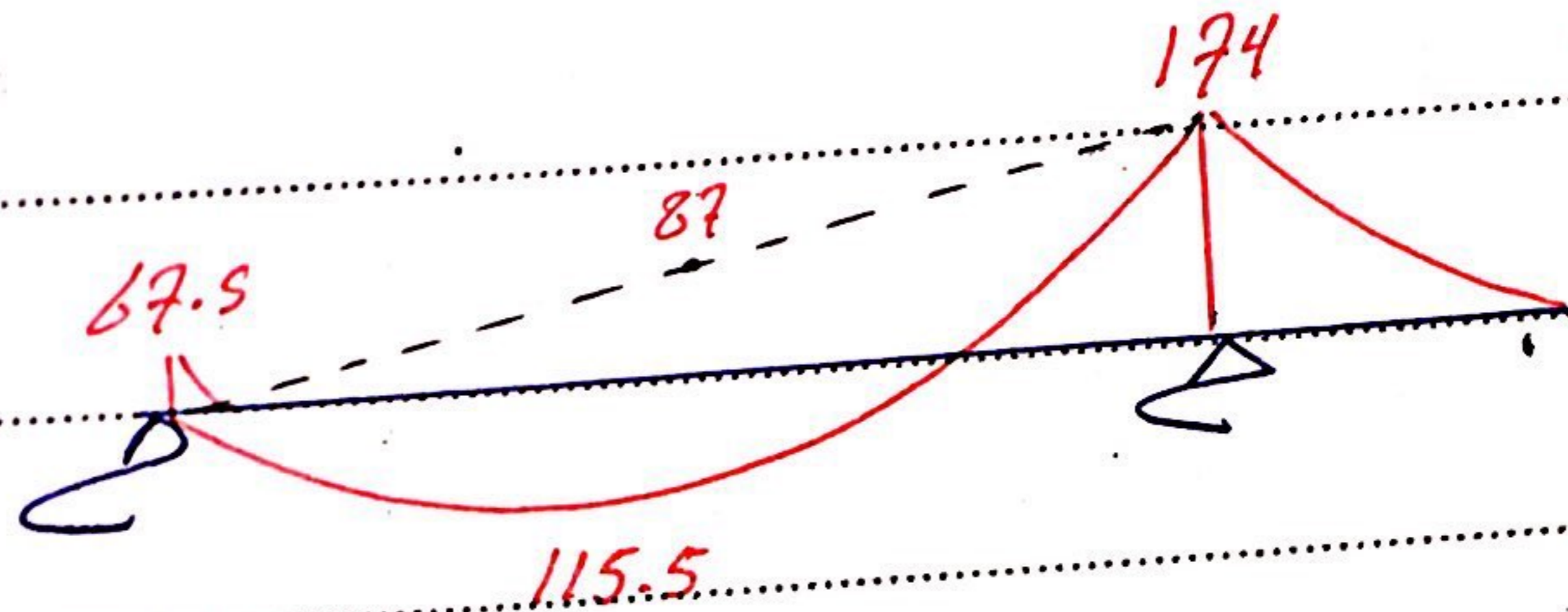
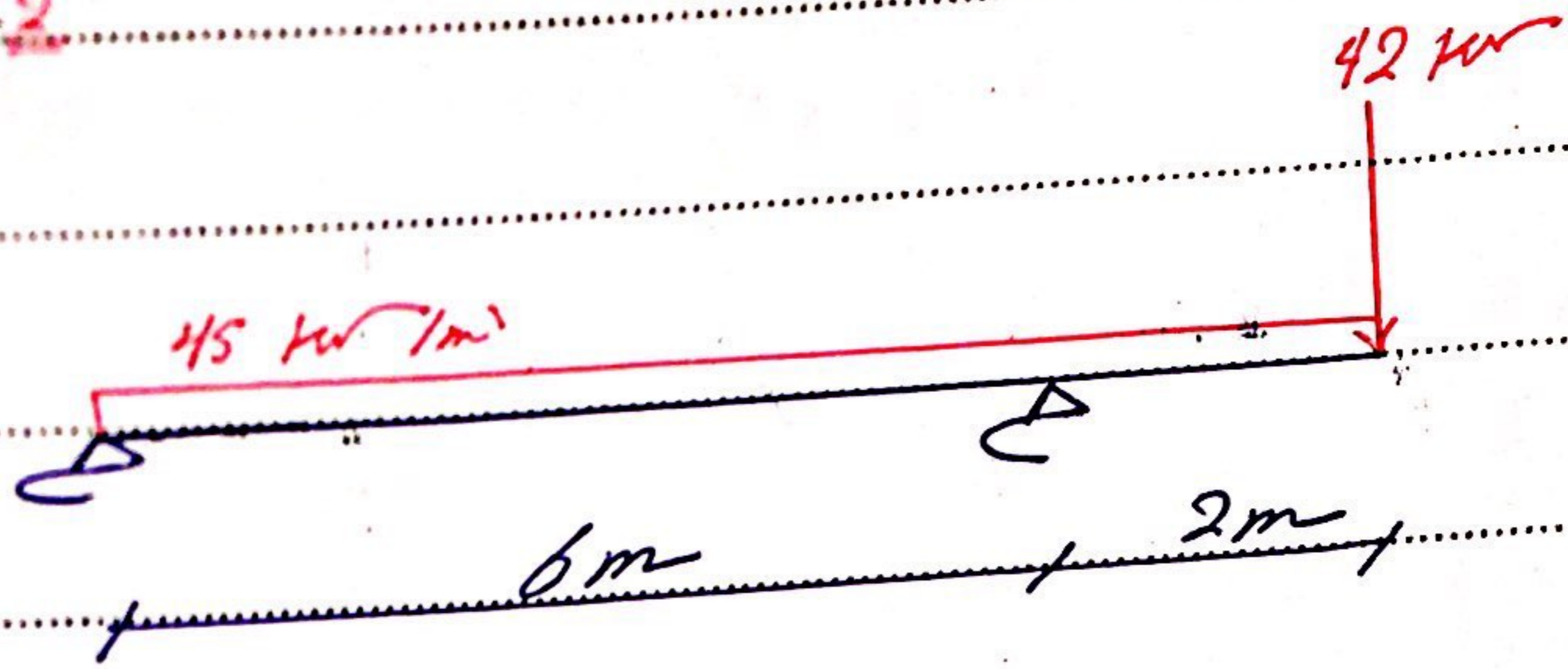
$$W_w = 3.75 + b + 8 \times 1.33 + 8 \times 1.5 \times \frac{2}{3} = 28.39 \text{ kN/m}$$

For part bc

$$W_w = 3.75 + b + 8 \times 1.33 = 20.39 \text{ kN/m}$$



Answer 2



Design For sec 1

$$b = 250 \text{ mm} \quad t = 500 \text{ mm}$$

$$d = 450 \text{ mm} \quad M_u = 174 \text{ kNm}$$

$$H.S.O. = \sigma_c \sqrt{\frac{174 \times 10^6}{25 \times 250}} \quad C_1 = 2.69 \text{ unsafe}$$

$$d = 3.5 \sqrt{\frac{174 \times 10^6}{25 \times 250}} = 583 \text{ mm}$$

$$\text{take } d = 600 \quad t = 650 \text{ mm}$$

$$C_1 = 3.59$$

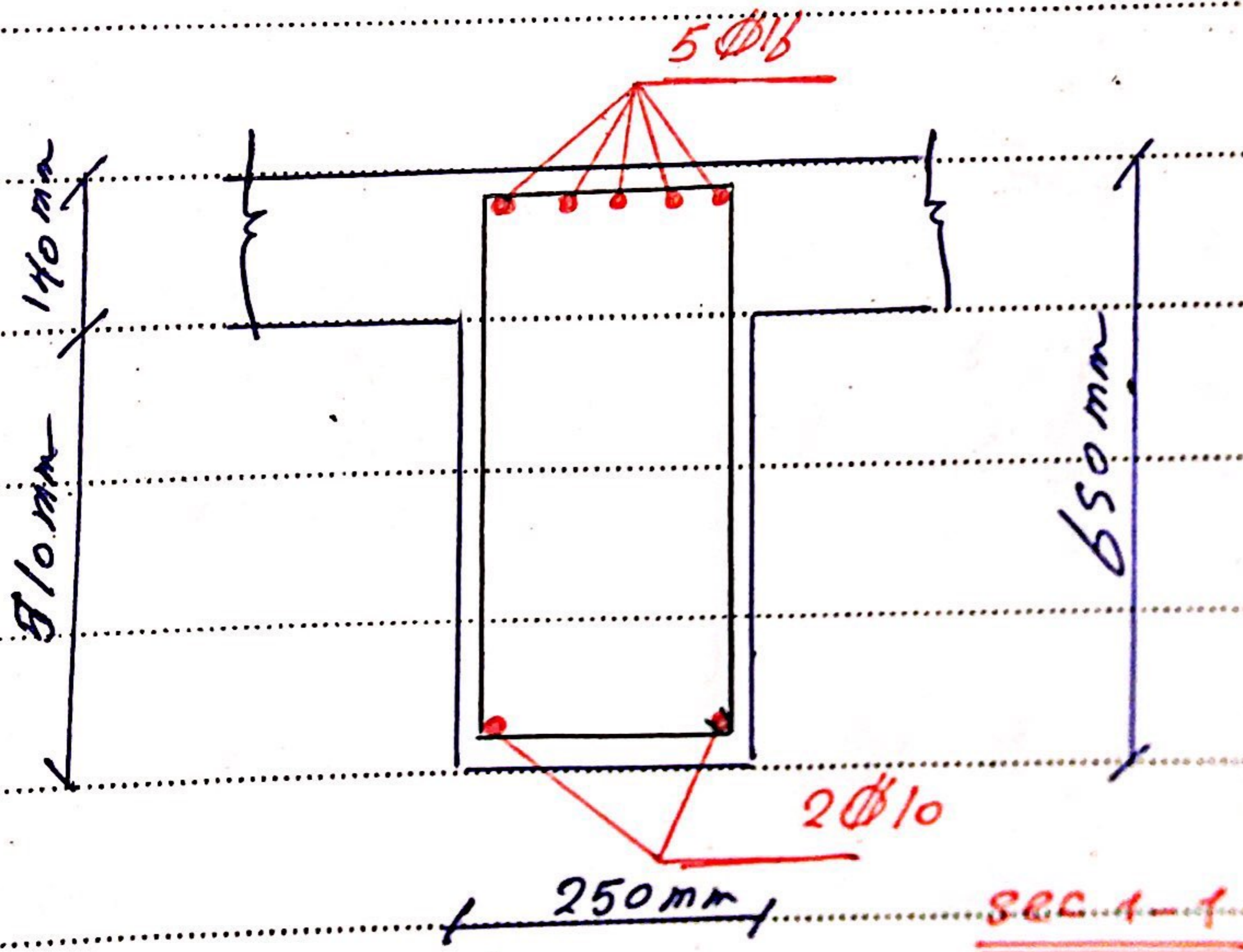
$$J = 0.782$$

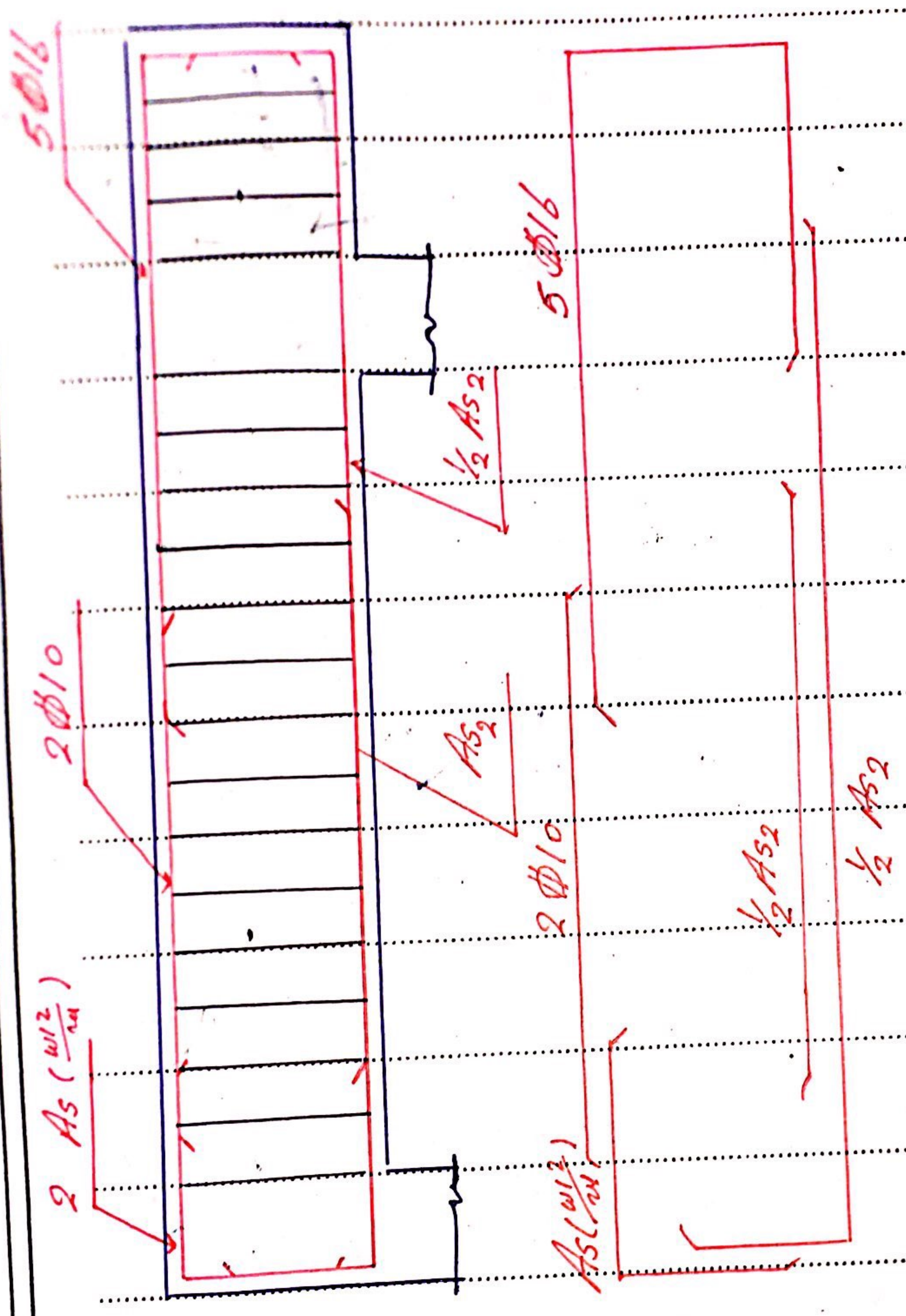
$$A_s = \frac{174 \times 10^6}{350 \times 0.782 \times 600} = 950 \text{ mm}^2$$

use 5  $\Phi 16$

$$A_{s_{min}} = \frac{1.1}{F_y} b d = 471.4 \text{ mm}^2$$

$$A_s' = (0.1 \sim 0.2) A_s = (95 \sim 190 \text{ mm}^2) = 2 \Phi 10$$





R.F.T (Elevation)